Estimating the lateral transfer of organic carbon through the European river 1 network using a land surface model

Table S1 Values of the key parameters used in the ORCHIDEE-C_{lateral} to simulate the lateral
transfer of sediment and carbon.

Parameter	Value	Unit	Description	Source
a	26.96	Unitless	Coefficient in Eq. 1	Calibrated
b	0.76	Unitless	Coefficient in Eq. 1	Calibrated
С	1.79	Unitless	Coefficient in Eq. 2	Calibrated
d	-0.065	Unitless	Coefficient in Eq. 2	Calibrated
Cebed	0.5	Unitless (0-1)	The fraction of sediment deficit that can be complemented by erosion of river bed (Eq. 6)	Calibrated
Cebank	0.5	Unitless (0-1)	The fraction of sediment deficit that can be complemented by erosion of river bank (Eq. 6)	Calibrated
Crivdep	0.1, 0.2, 0.5 ^{<i>a</i>}	Unitless (0-1)	Daily deposited fraction of the sediment surplus in stream reservoir (Eq. 5)	Calibrated
Cflddep	0.5, 1.0, 1.0 ^{<i>a</i>}	Unitless (0-1)	Daily deposited fraction of the sediment surplus in flooding reservoir (Eq. 11)	Calibrated
$P_{flooding}$	0.1	year	Return period of daily bankfull flow	Calibrated
$ au_{fast}$	3.0	day	A factor which translates the topographic index into the water residence time of the 'fast' reservoir (Eqs. 5, 6)	Guimberteau et al., 2012
$ au_{flood}$	1.4	day	A factor which translates the topographic index into the water residence time of the flooding reservoir (Eq. 18)	Guimberteau et al., 2012
$ au_{poc}$	0.3, 1.12, 0.3 ^b	year	A factor which translates the topographic index into the water residence time of the flooding reservoir (Eq. 25)	Lauerwald et al., 2017
ω	12.0, 5.0, 2.5 ^{<i>a</i>}	g s ⁻¹	Coefficient of proportionality for calculating sediment transport capacity (Eq. 8)	Calibrated

^{*a*} For clay, silt and sand sediment, respectively. ^{*b*} For active, slow and passive POC, respectively.

Abbreviation Discription Upstream drainage area (m²) A Fraction of sediment deficit that can be complemented by erosion of river bank each day (0-1, Cebank unitless) Fraction of sediment deficit that can be complemented by erosion of river bed each day (0-1, Cebed unitless) Daily deposited fraction of the suspended sediment in flooding waters (0-1, unitless) Cflddev Daily actual cover management factor (unitless, 0-1) Cidav Assumed reference cover management factor of MUSLE (unitless, 0-1) Cref Daily deposited fraction of the sediment surplus (0-1, unitless) Crivdep Drainage area of headwater basin i (m²) DAi DOC Dissolved organic carbon Evaporation of flooding water (m3 day⁻¹) Eh20 Fraction of floodplain area in each grid cell (0-1, unitless) fA fld Fraction of river surface in each grid cell (0-1, unitless) fA riv Transformation of sediment (k=sed, g day⁻¹) and POC (k= POC g C day⁻¹) deposited in river $F_{bed2fld k}$ channel to the floodplain soil Sediment (k=sed, g day⁻¹) or carbon (k= POC, DOC or CO₂, g C day⁻¹) entering the target Fbero_k river segment due to erosion of river bank Water $(k=h2o, m^3 day^{-1})$, sediment $(k=sed, g day^{-1})$ or carbon $(k=POC, DOC \text{ or } CO2, g C day^{-1})$ Fdown2fld k 1) flow from the target river segment to the neighbouring downstream floodplain Water $(k=h2o, m^3 day^{-1})$, sediment $(k=sed, g day^{-1})$ or carbon $(k=POC, DOC \text{ or } CO_2, g C day^{-1})$ Fdown2riv k 1) flow from the target river segment to the neighbouring downstream river Water $(k=h2o, m^3 day^{-1})$ or carbon $(k=DOC \text{ or } CO_2, g C day^{-1})$ flow from upland to the slow F_{DR k} water reservoir through drainage Water $(k=h2o, m^3 day^{-1})$, DOC $(k=DOC g C day^{-1})$ or CO2 $(k=CO2 g C day^{-1})$ infiltrated to F_{fd_k} floodplain soil, or sediment (k=sed, g day⁻¹) or POC ($k=POC \text{ g C day^{-1}}$) deposition on floodplain Water $(k=h2o, m^3 day^{-1})$, sediment $(k=sed, g day^{-1})$ or carbon $(k=POC, DOC \text{ or } CO_2, g C day^{-1})$ Ffld2riv_k ¹) input from flooding water to the target river segment Water $(k=h2o, m^3 day^{-1})$, sediment $(k=sed, g day^{-1})$ or carbon $(k=POC, DOC \text{ or } CO_2, g C day^{-1})$ FFout_k ¹) flow from fast reservoir to stream reservoir Daily decomposition rate of POC in water reservoir i (g C day⁻¹, i= fast, stream, flooding **F***рос* і water) Sediment (k=sed, g day⁻¹) or carbon (k= POC, DOC or CO₂, g C day⁻¹) deposition in river Frd k channel Frero_k Sediment (k=sed, g day⁻¹) or carbon (k= POC, DOC or CO₂, g C day⁻¹) entering the target river segment due to erosion of river bed Water $(k=h2o, m^3 day^{-1})$, sediment $(k=sed, g day^{-1})$ or carbon $(k=POC, DOC \text{ or } CO_2, g C day^{-1})$ FRO k 1) flow from upland to the fast water reservoir through surface runoff Topographic index of each headwater basin (unitless) ftopo Water $(k=h2o, m^3 day^{-1})$, sediment $(k=sed, g day^{-1})$ or carbon $(k=POC, DOC \text{ or } CO_2, g C day^{-1})$ Fup2fld_k 1) flow from upstream river segment to the neighbouring downstream floodplain Water (k=h2o,m³ day⁻¹), sediment (k=sed, g day-1) or carbon (k=POC, DOC or CO_2 , g C day-Fup2riv k 1) input from upstream river segments to the target river segment Infiltration of flooding water (m³ day⁻¹) Ih20

10 **Table S2** Abbreviation used in this study.

Ki	Soil erodibility factor of MUSLE in headwater basin <i>i</i> (Mg MJ ⁻¹ mm ⁻¹)			
LSi	The combined dimensionless slope length and steepness factor MUSLE in headwater basin <i>i</i> (<i>unitless, 0-1</i>)			
PFT	Plant functional type			
POC	Particulate organic carbon			
POCa	Active POC pool			
POC _p	Passive POC pool			
POCs	Slow POC pool			
Pref	Factor of erosion control practices (unitless, 0-1)			
q ave	Long-term average stream flow rate (m ³ s ⁻¹)			
q i_ref	Daily peak flow rate at the outlet of headwater basin <i>i</i> under the assumed reference runoff condition $(m^3 s^{-1})$			
Q_{i_ref}	Total water discharge at the outlet of headwater basin <i>i</i> for the daily reference runoff condition $(m^3 day^{-1})$			
q iday	Stream flow rate on day $i(m^3 s^{-1})$			
R_{30_k}	The maximum half-hour runoff in each day (mm 30-min ⁻¹)			
R _{30_ref}	Assumed reference daily maximum 30-minutes runoff (mm 30-min ⁻¹)			
R iday	Daily total surface runoff (mm day ⁻¹)			
R _{ref}	Assumed reference daily total runoff (= 10 mm day^{-1})			
Sdeep	Soil layer under 2 m depth			
S _{fast_k}	Water ($k=h2o$,m ³), sediment ($k=sed$, g) or carbon ($k=POC$, DOC or CO_2 , g C) storage in the fast water reservoir (i.e. the upland surface runoff)			
S_{fld_k}	Water $(k=h2o,m^3)$, sediment $(k=sed, g)$ or carbon $(k=POC, DOC \text{ or } CO_2, g C)$ storage in the			
Si_ref	The problem is the problem in the problem is the problem in the problem in the problem is the p			
S_{iday}	Actual daily sediment delivery from land to river a specific $0.5^{\circ} \times 0.5^{\circ}$ grid cell (g day ⁻¹ grid ⁻¹)			
SOC	Soil organic carbon			
Spoc_i	Stock of POC in each water reservoir (g C day ⁻¹ , i = fast, stream, flooding water)			
Sref	Total sediment delivery from land to river in a specific $0.5^{\circ} \times 0.5^{\circ}$ grid cell under reference runoff and vegetation cover conditions (g dav-1 grid-1)			
Sriv_k	Water ($k=h2o$,m ³), sediment ($k=sed$, g) or carbon ($k=POC$, DOC or CO^2 , g C) storage in the stream water reservoir			
ТС	Sediment transport capacity (g m ⁻³)			
ТОС	Total organic carbon			
Twater	Temperature of water reservoirs (°C)			
T fast	Default water residence time of the fast reservoir (= 3 days)			
$ au_{flood}$	Default water residence time of the flooding water reservoir (= 3 days)			
$ au_{POC_i}$	the turnover time of the <i>i</i> (active, slow and passive) POC pool (year)			
ω	Coefficient of proportionality for calculating sediement transport capacity (unitless)			

12 Figures in Supplementary Information

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Figure S1 Comparison between the return period of daily bankfull flow ($P_{flooding}$) and the return period of flooding event. When the threshold of bankfull flow is set to 4550 m³ s⁻¹, $P_{flooding}$ showed in this figure is 0.1 year as the bankfull flow occurred in 20 days during the investigated term of two years. But the return period of flooding event is 0.5 year as there are four flooding events.





Figure S2 Geographical location of the gauging stations for river discharge (a), bankfull flow (b), sediment discharge (c) and riverine organic carbon discharge (d) used in this. Figure (d) also shows the spatial distribution of 57 catchments in Europe. The simulated average net soil loss rates (g m⁻² yr⁻¹) at these 57 catchments were compared to the average net soil loss rates extracted from the sediment delivery data provided by the ESDAC (see section 2.3 of the main text).



Figure S3 Relative changes in simulated riverine sediment and carbon discharges with 10%

31 increase and decrease in parameters controlling sediment transport in river network. ω is the

32 coefficient of proportionality for calculating sediment transport capacity (Eq. 8); c_{flddep} is the

daily deposited fraction of the sediment surplus in flooding reservoir (Eq. 11); *c*_{rivdep} is the daily

deposited fraction of the sediment surplus in stream reservoir (Eq. 5); *c*_{ebank} is the fraction of

sediment deficit that can be complemented by erosion of river bank (Eq. 6); *c*_{ebed} is the fraction

of sediment deficit that can be complemented by erosion of river bed (Eq. 6);



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Figure S4 Comparison between the simulated and observed time series of mean annual water

discharge rates at 14 gauging stations.



42 Figure S5 (a) Comparison between the river network extracted from the STN-30p database at

43 0.5° resolution (blue) (i.e. the forcing data of stream flow directions used in this study) and the

44 river network derived from the HydroSHEDS DEM data at 3" resolution (red); (b) the real river

45 network in the estuary region of the Danube River (obtained from © Google Maps). GRDC_ID

denotes the identify number of the gauging station in the GRDC database (Table 1).



Figure S6 Comparison between the simulated SOC stock by ORCHIDEE-Clateral and those
obtained from five soil databases. Figure (a) and (b) showed the SOC stocks in the 0-0.3 m and
0-1.0 m soil layer, respectively. Value in the legend following the name of each soil database is
the total SOC stock in the whole Europe. Sources of the soil databases used in this figure can be
found in Table 1.



Figure S7 Comparison between the simulated and observed total organic carbon (TOC)

concentrations in representative European rivers. DA is the drainage area of the correspondinggauging station.



Figure S8 Comparison between the simulated and observed dissolved organic carbon (DOC)
 concentrations in representative European rivers. DA is the drainage area of the corresponding
 gauging station.



Figure S9 Land cover fraction of forest, grassland, cropland and bare soil (e.g. desert,

- 66 waterbodies and bare rock) in each $0.5^{\circ} \times 0.5^{\circ}$ grid cell in Europe during the period 1901-2014.
- 67 For the Europe, the land cover fraction of forest, grassland, cropland and bare soil are 30.0%,
- 68 41.1%, 21.1% and 7.8%, respectively.



Figure S10 Spatial distribution of elevation (a) and floodplains (b) in Europe. Elevation and
floodplain distribution data are obtained from the ASTER GDEM v3 (Abrams et al., 2020) and

73 GFPLAIN250m (Nardi et al., 2019), respectively.



Figure S11 The simulated time series of annual total sediment delivery from upland to river network (a), DOC and POC delivery from land to river network (b), vegetation net primary production (NPP, c), heterotrophic respiration (Rh, d), respiration due to disturbances like harvest and land cover change (Rd, e), changes in living biomass (f), changes in litter carbon stock (g) and changes in SOC stock (h) in whole Europe from the year 1901 to 2014.



Figure S12 The simulated time series of living vegetation biomass (a), litter carbon pool (b) and

total soil organic carbon pool (SOC+DOC, c) by ORCHIDEE-C_{lateral} and ORCHIDEE (i.e.

84 ORCHIDEE-C_{lateral} with deactivated soil erosion and routing module) in whole Europe from the

year 1901 to 2014. The blue line in each subplot is the difference between the simulated results

86 from ORCHIDEE-C_{lateral} and ORCHIDEE.



Figure S13 Changes in soil temperature (Tem, °C) and soil wetness (SW, unitless) above wilting
point due to the lateral carbon transport. The change of Tem was calculated as Tem_{lat} - Tem_{nolat},
where Tem_{lat} and Tem_{nolat} are the soil temperatures when lateral carbon transport is considered
and ignored, respectively. The change of SW was calculated in the same method as the Tem.